

Ex) Same as above, but now, a bank of 12 tubes...

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$$3 \times 4 \begin{Bmatrix} \circ & \circ & \circ & \circ \\ \circ & \circ & \circ & \circ \\ \circ & \circ & \circ & \circ \end{Bmatrix} \quad h_{\text{horiz}, N \text{ tubes}} = \frac{h_{\text{horiz}, 1 \text{ tube}}}{N^{1/4}} \quad \left(N \approx 3 \right)$$

$$= 7042 \text{ W/m}^2\text{K} \quad \text{for each } \begin{Bmatrix} \circ \\ \circ \\ \circ \end{Bmatrix} \text{ bank}$$

↓

$$A_{\text{surf}} \text{ for all 12 tubes} = N_{\text{total}} (\pi D L) = 1.131 \text{ m}^2$$

↑ 12 ↑ 0.03 m ↑ 1 m

so

$$\dot{Q} = h A_{\text{surf}} (T_{\text{sat}} - T_s) = 79,870 \text{ W}$$

↑ ↑
40°C 30°C

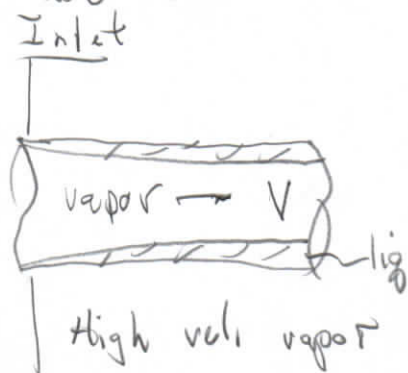
and the rate of steam cond. is

$$\dot{m}_{\text{cond.}} = \frac{\dot{Q}}{h_{\text{fg}}} = \frac{79,870 \text{ W}}{2435 \times 10^3 \text{ J/kg}} = 0.0328 \text{ kg/s}$$

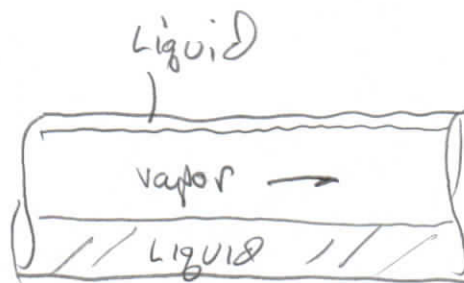
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what about cond. inside tubes?

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upto



Low velocity vapor

$$h_{\text{internal horiz}} = 0.555 \left[\frac{sg_L (\rho_L - \rho_v) k_L^3}{\mu_L (T_{\text{sat}} - T_s) D} \left(h_{fg} + \frac{3}{8} C_{p,L} (T_{\text{sat}} - T_s) \right) \right]^{1/4}$$

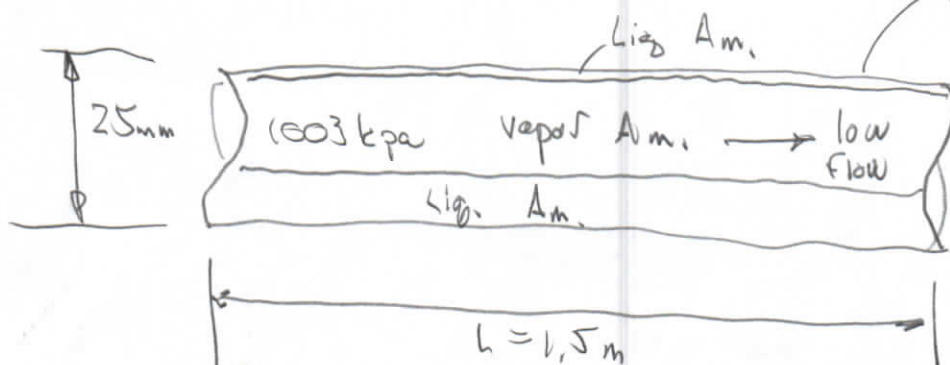
just an h_{fg}^*
 $\uparrow$ $\frac{Chato}{for}$

for $Re_{\text{vapor}} = \frac{\rho_v V_{\text{in}} D}{\mu_v} \Big|_{\text{inlet}} < 35,000$

Low Velocities

See Rohsenow for high speed flow.

Ex | Vapor ammonia $\rightarrow$ Liq. Ammonia
 bad for Ca. NOT as bad



$T_{\text{surf}} = 15^\circ\text{C}$ (constant!)

Calc. in to have fully cond. Am. at end of the 1.5 m tube, $< 35,000$ (verify this)

Assume • (55)

• Tube is (T)

• "low flow" so Re_{vapor}

Prop. For Am. ② $P = 1003 \text{ kPa}$, $T_{\text{sat.}} = 25^\circ\text{C}$

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$$\textcircled{3} T_{\text{sat}} = 25^\circ\text{C}, \quad h_{fg} = 1166 \times 10^3 \text{ J/kg}$$

$$S_w = 7.809 \text{ kg/m}^3$$

$$\mu_w = 1.037 \times 10^{-5} \text{ kg/ms}$$

$$\textcircled{4} T_{F,lm} = \frac{T_{\text{sat}} + T_s}{2} = \frac{(25 + 15)^\circ\text{C}}{2} = 20^\circ\text{C} \quad \text{we can find}$$

$$S_l = 610.2 \text{ kg/m}^3$$

$$C_{p,l} = 4745 \text{ J/kg K}$$

$$\mu_l = 1.519 \times 10^{-4} \text{ kg/m}^2$$

$$k_l = 0.4927 \text{ W/mK}$$

Calculations

$$h_{\text{horiz tube}} = 0.555 \left[\frac{g S_l (S_l - S_w) k_l^3}{\mu_l (T_{\text{sat}} - T_s) D} \left(h_{fg} + \frac{3}{8} C_{p,l} (T_{\text{sat}} - T_s) \right) \right]^{1/4}$$

$h_{fg}^* = 1183.8 \times 10^3 \text{ J/kg}$

$$= 5976.3 \text{ W/m}^2\text{K}$$

Surface area $= A_s = \pi D L = 0.11781 \text{ m}^2$
for h_{transf}

$$\text{So } Q = h A_s (T_{\text{sat}} - T_s) = 7046 \text{ W}$$

$$\text{Rate of cond } \dot{m} = \frac{Q}{h_{fg}} = 0.005948 \text{ kg/s}$$

keep in below
this valve for
Full condensation

$$\text{Note: } Re_{\text{vapor}} = \frac{8 V_w D}{\mu_w} \Big|_{\text{inlet}} = \frac{4 \dot{m}}{\pi D \mu_w} = 29,212 < 35,000$$

// so low flow assum. is okay.